



Original Article

# Structure and Magnetic Properties of SrFe<sub>12</sub>O<sub>19</sub>/CoFe<sub>2</sub>O<sub>4</sub> Nanocomposite Ferrite

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**Abstract:** Nanocomposite particles SrFe<sub>12</sub>O<sub>19</sub>/ CoFe<sub>2</sub>O<sub>4</sub> were synthesized by sol-gel method. The nanocomposites are formed at the calcining temperature around 850 °C in 5 hours. The phase composition, surface morphology and magnetic properties of the nanocomposites were investigated using XRD, SEM and VSM, respectively. The results show that the magnetic properties of nanocomposite particles are strongly influenced by the molar ratios of the hard and soft phases and particle size distributions. The samples with the mass ratio of  $R_m = \text{SrFe}_{12}\text{O}_{19} / \text{NiFe}_2\text{O}_4 = 1/3$  and  $1/5$  are characterized with a “bee waist” type hysteresis loop. While all the samples  $R_V$  show an excellent smooth hysteresis loop and a single – phase magnetization behavior. The coercivity decreases significantly and the magnetization drastically increases with decreasing of volume ratio  $R_V$ .

**Keywords:** nanocomposite, sol- gel method, exchange coupling.

## 1. Introduction

Nanocomposite magnetic materials consisting of soft and hard magnetic phases have become a hot research topic in recent time because of potential applications in the fields of science and technology. For example, magnetic micro electromechanical systems (MEMS) including microactuators, sensors, recording heads and micro-motors, spins of electron devices apply in spin- valve read heads [1-4]. Theoretically, by combining high magnetic anisotropy of magnetically hard phase and the high saturation magnetization of magnetically soft phase can enhance their magnetic properties. However,

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the magnetic properties of nanocomposite materials depend strongly on the grain size, structure and morphology of phases, distribution of the magnetically hard and soft phases, and impurity. Numerous efforts have recently been made into the fabrication of nanocomposite particles to enhance exchange coupling interaction by controlling the particle size and distribution particles. Among the hard materials (NdFeB, SmCo<sub>5</sub>, FePt...), strontium ferrite (SrM) has high coercivity  $H_C$ , large magneto-crystalline anisotropy [5] and excellent chemical stability [6]. It is well known that CoFe<sub>2</sub>O<sub>4</sub> is a spinel ferrite, which possesses higher saturation, remanent magnetization and coercivity compared with other spinel ferrites (NiFe<sub>2</sub>O<sub>4</sub>, MnFe<sub>2</sub>O<sub>4</sub>, ...) [7]. Therefore, in the exchange spring magnet, mixing of SrM- hard phase and CoFe<sub>2</sub>O<sub>4</sub> phase could utilize the superior magnetic properties of two phases. The recent research work showed that the ferrite particles can be obtained via the chemical methods such as coprecipitation, hydrothermal [8, 9], sol-gel [10, 11]. Moreover, the ferrites can be successfully synthesized at a relatively low temperature without subsequent sintering at high temperature. That may be beneficial to control the growth of crystallites. So, we only need a relatively lower sintering temperature to achieve the homogeneous ferrite particles and a strong exchange coupling. In this work, SrFe<sub>12</sub>O<sub>19</sub>/CoFe<sub>2</sub>O<sub>4</sub> nanocomposite have been prepared by sol-gel method.

## 2. Experiment

### *Synthesis of SrFe<sub>12</sub>O<sub>19</sub> and CoFe<sub>2</sub>O<sub>4</sub> powders*

SrFe<sub>12</sub>O<sub>19</sub> and CoFe<sub>2</sub>O<sub>4</sub> nanopowders were synthesized separately by via sol-gel method. Fe(NO<sub>3</sub>)<sub>3</sub>·9H<sub>2</sub>O, Sr(NO<sub>3</sub>)<sub>2</sub> and Co(NO<sub>3</sub>)<sub>2</sub>·6H<sub>2</sub>O were dissolved in deionized water to form an aqueous solution of 1M. The nitrates used to synthesize SrFe<sub>12</sub>O<sub>19</sub> and CoFe<sub>2</sub>O<sub>4</sub> were dissolved in deionized water with the molar ratio Sr/Fe is 11.5 and Co/Fe is 2. Citric acid (AC) was then added into the solution at fixed [Sr<sup>2+</sup> + Fe<sup>3+</sup>]:AC and [Co<sup>2+</sup> + Fe<sup>3+</sup>]: AC molar ratio of 1:3. NH<sub>4</sub>OH was used to adjust the pH to 1. After the pH had been stabilized, the solution was stirred at 1000 rpm and gradually evaporated at 90 °C. As the water evaporated, the remainder became highly viscous gels as a result of the chelation process. These gels were dried at 90 °C for 24 h, and then heated at 450 °C (for SrFe<sub>12</sub>O<sub>19</sub>) and 200 °C (for CoFe<sub>2</sub>O<sub>4</sub>) for 2 hours to eliminate the remaining residual water and other organic impurities (aerogels were formed). To form the hexaferrite and spinel phase, the gels were calcined in air at 850°C for 5 hours.

### *Preparation of SrFe<sub>12</sub>O<sub>19</sub>/CoFe<sub>2</sub>O<sub>4</sub> nanocomposites*

The first series of specimens SrFe<sub>12</sub>O<sub>19</sub>/CoFe<sub>2</sub>O<sub>4</sub> nanopowders were synthesized using the aerogel powders obtained previously. SrFe<sub>12</sub>O<sub>19</sub> and CoFe<sub>2</sub>O<sub>4</sub> aerogel powders were uniformly mixed with mass ratios ( $R_m$ ) of 1:1, 1:3, 1:5 and 1:7, denoted as  $R_{m11}$ ,  $R_{m13}$ ,  $R_{m15}$  and  $R_{m17}$ , respectively. Then the mixtures were pressed into platelets of 6 mm in diameter and sintered at 850 °C for 5 hours.

The second series of specimens, the SrFe<sub>12</sub>O<sub>19</sub>/CoFe<sub>2</sub>O<sub>4</sub> nanocomposite powders were synthesized by one step sol-gel method. Stoichiometric amounts of Fe(NO<sub>3</sub>)<sub>3</sub>·9H<sub>2</sub>O, Sr(NO<sub>3</sub>)<sub>2</sub>, Co(NO<sub>3</sub>)<sub>2</sub> were dissolved completely in deionized water. In these processes, the ratio of Sr<sup>2+</sup>/Fe<sup>3+</sup> and Fe<sup>3+</sup>/Co<sup>2+</sup> were fixed at 11.5 and 2. The ratio  $R_v$  of (Sr<sup>2+</sup>/Fe<sup>3+</sup>) : (Fe<sup>3+</sup>/Co<sup>2+</sup>) was fixed at 1:1, 1:3, 1:5 and 1:7. Citric acid was then added into the solution at a fixed (Sr<sup>2+</sup> + Fe<sup>3+</sup> + Co<sup>2+</sup>)/AC volume ratio of 1/3. NH<sub>4</sub>OH in aqueous form was added to the mixed solutions and the pH of the solutions was adjusted to about 1. The mixtures were stirred at 1000 rpm and slowly evaporated at 90 °C to form gels. These gels were dried at 90 °C for 24 h and then heated at 350 °C for 2 hours to eliminate the remaining residual water and other organic impurities. An equal weight of the produced ferrite powders was compressed into

briquettes of 6 mm diameters and 3 g weight. The composites were annealed in air at 850 °C for 5 h. The samples were marked as  $R_{v11}$ ,  $R_{v13}$ ,  $R_{v15}$  and  $R_{v17}$ .

### Characterization

The crystal structure and phases of the obtained samples were identified via X-ray powder diffraction (XRD) using a Siemens D5000 diffractometer ( $\text{CuK}\alpha$  radiation,  $\lambda = 1.54056 \text{ \AA}$ ). Morphological features and particle size were observed by scanning electron microscopy (SEM, JEOL-JSM 7600F). The magnetic were measured using a vibrating sample magnetometer (VSM, Lakeshore 7410) with applied magnetic fields up to 10 kOe. Thermogravimetric analyses (TGA) were employed to study thermal behavior using a Universal V2960T with a heating rate of 10 °C/min in air, whereas pure alumina powder was used as the reference specimen.

### 3. Result and discussions

The TGA of gel precursor with  $R_v = 1$  are shown in the Fig. 1. The experiment was performed using 23.224 mg of gel precursor and a heating of 10 °C/ min in static air. The first exothermic peak at approximately 152 °C was attributed to the decomposition of  $\text{NH}_4\text{NO}_3$  to liberate  $\text{NO}$ ,  $\text{O}_2$ , and  $\text{H}_2\text{O}$  and the weight loss of 45%. The second exothermic peak at approximately 230 °C showed the decomposition of the remaining unreactive organic material induced by excess citric and weight loss of 67.4% (Fig. 1 a). At the approximately 549 °C and 730 °C, the weight loss about 70.55% (Fig. 1 b). At higher temperature, the weight has not decreased. Based on the results obtained from the thermal analysis of the composite precursor (Fig. 1), we choose the temperature of 350 °C for heating gels and eliminating the remaining residual water and other organic impurities.

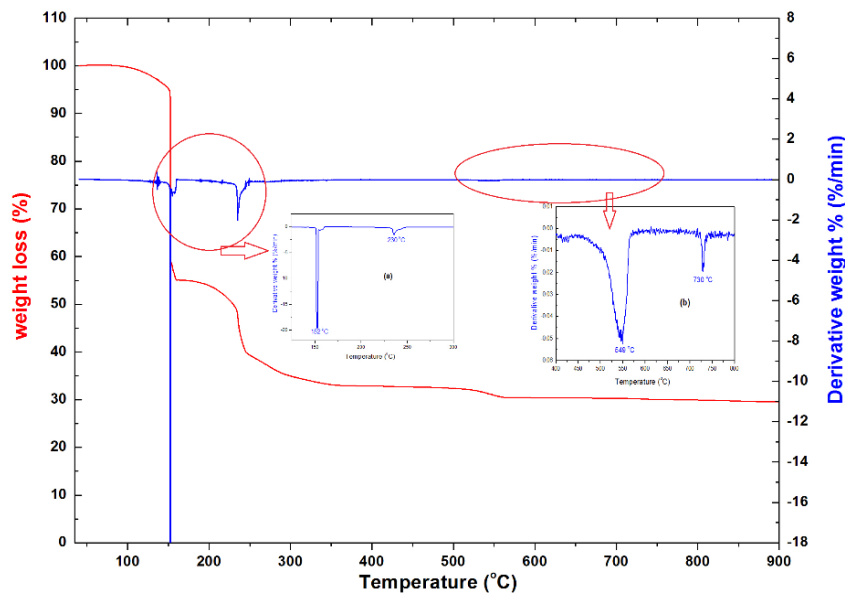


Figure 1. Thermogravimetric (TGA) curve of the gel precursor at  $R_v = 1$ .

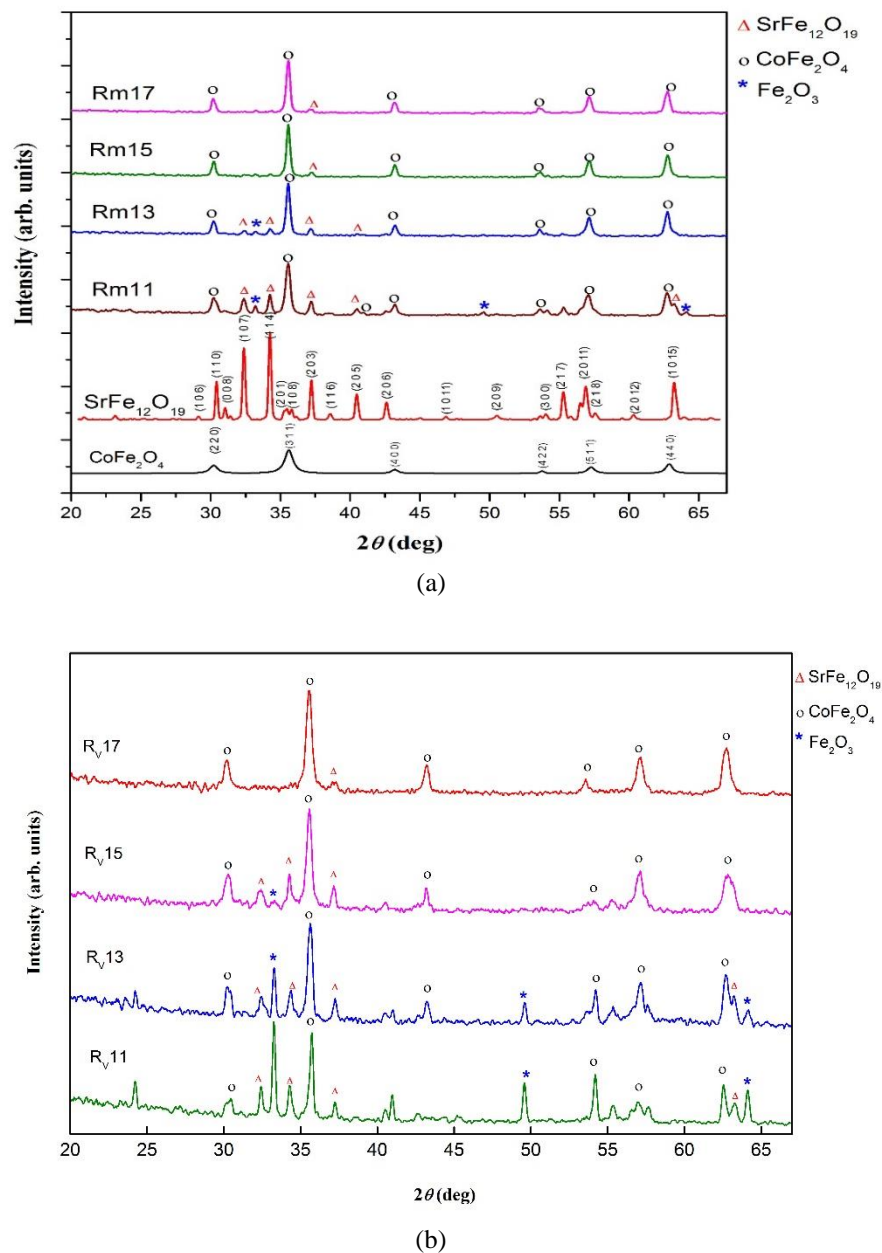


Figure 2. XRD patterns of the SrFe<sub>12</sub>O<sub>19</sub>/CoFe<sub>2</sub>O<sub>4</sub> nanocomposite powders calcination at 850 °C for 5 hours (a) R<sub>m</sub> and (b) R<sub>v</sub>.

The XRD patterns of the SrFe<sub>12</sub>O<sub>19</sub>, CoFe<sub>2</sub>O<sub>4</sub> and SrFe<sub>12</sub>O<sub>19</sub>/CoFe<sub>2</sub>O<sub>4</sub> nanocomposites powders with various of R<sub>m</sub> and R<sub>v</sub> are shown in the Fig.2. It can be clearly seen that the SrFe<sub>12</sub>O<sub>19</sub> and CoFe<sub>2</sub>O<sub>4</sub> samples are single phase after calcination at 850 °C for 5 hours. While all nanocomposite samples composed of SrFe<sub>12</sub>O<sub>19</sub>, CoFe<sub>2</sub>O<sub>4</sub> phases and a small amount of impurity phase of α- Fe<sub>2</sub>O<sub>3</sub>. This observation was also reported by other authors and may be attributed to the occurrence of local combustion during calcination [12, 13]. XRD refinements were carried out using the Rietveld method

with the help of the Fullprof program. The percentages of phases present in these samples and lattice parameters ( $a$ ,  $c$ ) are listed in Table 1. The percentages of  $\alpha$ -Fe<sub>2</sub>O<sub>3</sub> impurity phase decreases with increasing of concentration CoFe<sub>2</sub>O<sub>4</sub> at all nanocomposite samples. According to Wei Zhong et al. [14], the preliminary heating process at temperatures between 300 °C and 500 °C could further enhance the development of Sr-ferrite after calcination and remove  $\alpha$ -Fe<sub>2</sub>O<sub>3</sub> impurity phase. For  $R_m$  samples, the aerogels of SrFe<sub>12</sub>O<sub>19</sub> and CoFe<sub>2</sub>O<sub>4</sub> were heated at 450 °C and 200 °C before mixing. And for  $R_v$  samples, the aerogels of nanocomposite samples were heated at 350 °C. Therefore, the percentage of  $\alpha$ -Fe<sub>2</sub>O<sub>3</sub> impurity phase in  $R_m$  samples are smaller than that of  $\alpha$ -Fe<sub>2</sub>O<sub>3</sub> impurity phase in  $R_v$  samples. It can be concluded that using the sol – gel method to prepare nanocomposite samples need higher preliminary heating temperature (>350 °C).

Table 1. Lattice parameters ( $a$ ,  $c$ ) and percentages of phases present in the obtained samples

Sample	Phase	$a$ (Å)	$c$ (Å)	%
SrFe <sub>12</sub> O <sub>19</sub>	SrFe <sub>12</sub> O <sub>19</sub>	5,8723	23,0247	
CoFe <sub>2</sub> O <sub>4</sub>	CoFe <sub>2</sub> O <sub>4</sub>	8,398		
$R_m$ 11	SrFe <sub>12</sub> O <sub>19</sub>	5,873	23,024	42,58
	CoFe <sub>2</sub> O <sub>4</sub>	8,312		48,59
	$\alpha$ -Fe <sub>2</sub> O <sub>3</sub>			8,83
$R_m$ 13	SrFe <sub>12</sub> O <sub>19</sub>	5,8752	23,018	21,76
	CoFe <sub>2</sub> O <sub>4</sub>	8,326		71,21
	$\alpha$ -Fe <sub>2</sub> O <sub>3</sub>			7,03
$R_m$ 15	SrFe <sub>12</sub> O <sub>19</sub>	5,8754	23,023	8,80
	CoFe <sub>2</sub> O <sub>4</sub>	8,3305		83,65
	$\alpha$ -Fe <sub>2</sub> O <sub>3</sub>			7,55
$R_m$ 17	SrFe <sub>12</sub> O <sub>19</sub>	5,8736	23,017	2,90
	CoFe <sub>2</sub> O <sub>4</sub>	8,3218		91,13
	$\alpha$ -Fe <sub>2</sub> O <sub>3</sub>			5,97
$R_v$ 11	SrFe <sub>12</sub> O <sub>19</sub>	5,8765	23,027	36,29
	CoFe <sub>2</sub> O <sub>4</sub>	8,3313		11,32
	$\alpha$ -Fe <sub>2</sub> O <sub>3</sub>			52,39
$R_v$ 13	SrFe <sub>12</sub> O <sub>19</sub>	5,8781	23,03	34,63
	CoFe <sub>2</sub> O <sub>4</sub>	8,3135		39,30
	$\alpha$ -Fe <sub>2</sub> O <sub>3</sub>			26,7
$R_v$ 15	SrFe <sub>12</sub> O <sub>19</sub>	5,873	23,027	38,24
	CoFe <sub>2</sub> O <sub>4</sub>	8,326		47,47
	$\alpha$ -Fe <sub>2</sub> O <sub>3</sub>			14,03
$R_v$ 17	SrFe <sub>12</sub> O <sub>19</sub>	5,8756	23,0168	7,41
	CoFe <sub>2</sub> O <sub>4</sub>	8,323		92,59
	$\alpha$ -Fe <sub>2</sub> O <sub>3</sub>			0

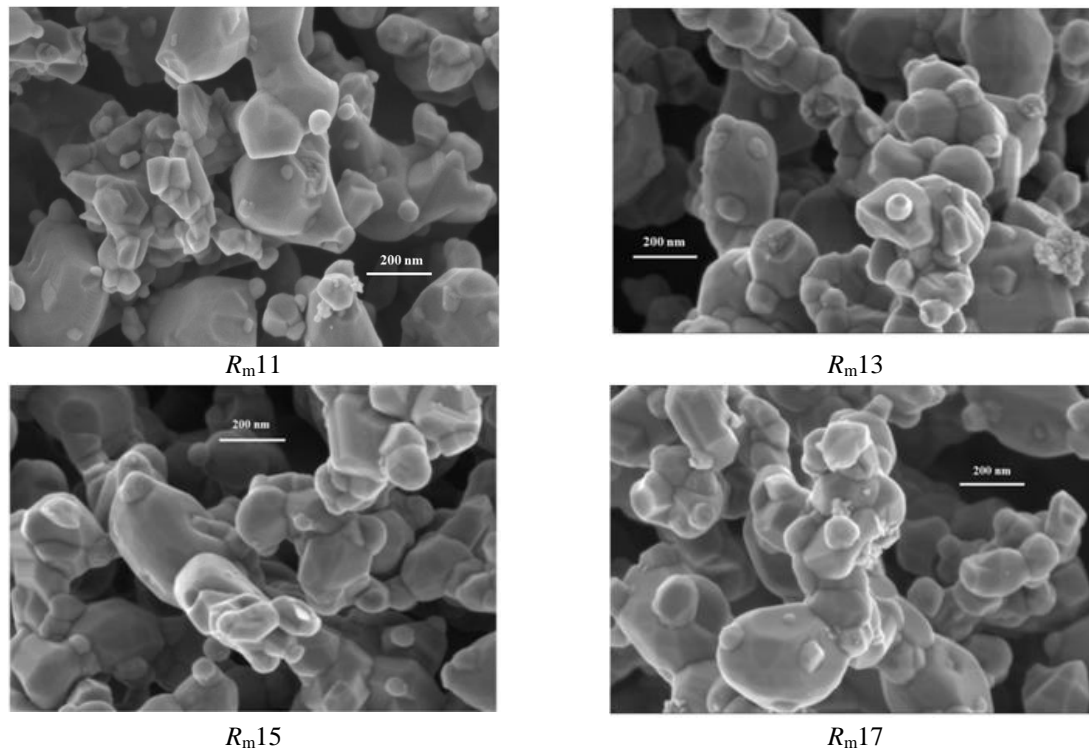


Figure 3. SEM images of the SrFe<sub>12</sub>O<sub>19</sub>/CoFe<sub>2</sub>O<sub>4</sub> nanocomposite samples with different mass ratios ( $R_m$ ) calcinated at 850 °C for 5 h.

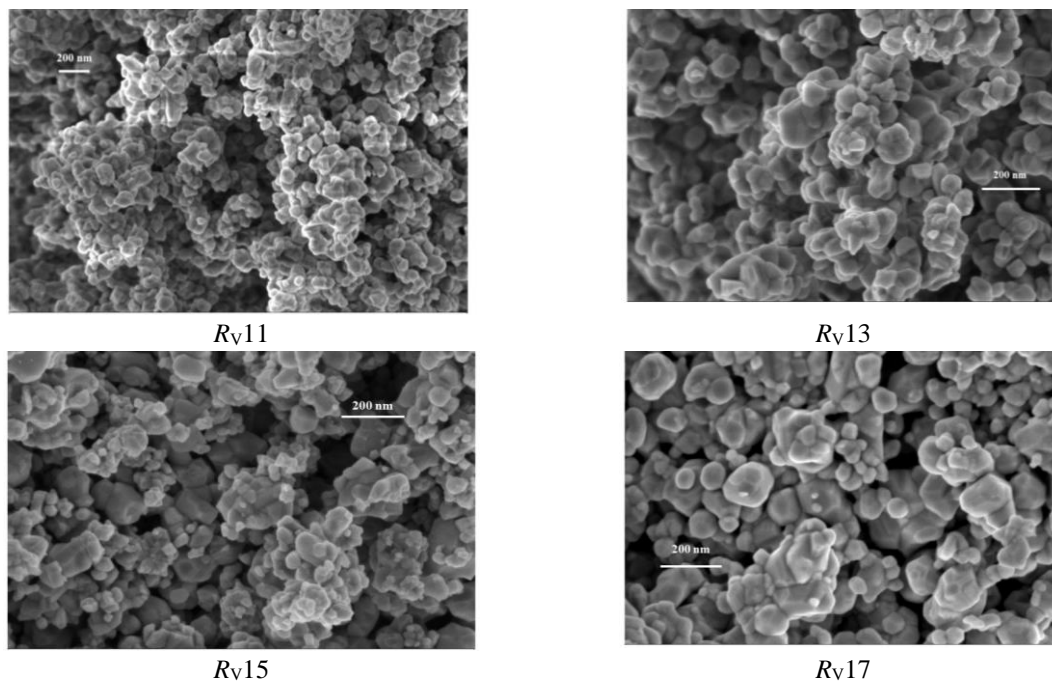


Figure 4. SEM images of the SrFe<sub>12</sub>O<sub>19</sub>/CoFe<sub>2</sub>O<sub>4</sub> nanocomposite samples with different volume ratios ( $R_v$ ) calcinated at 850 °C for 5 h.

The SEM images of SrFe<sub>12</sub>O<sub>19</sub>/CoFe<sub>2</sub>O<sub>4</sub> nanocomposites with different mass and volume ratios of phases are illustrated in Fig. 3 and 4. Fig. 3 shows SEM micrographs of  $R_m$  samples. We can see that cubic grains with smaller size are distributed in a matrix of hexagonal grains with larger size. The hexagonal plate-like and cubic grains have approximate diameter from 50 nm to 100 nm and 30 nm to 50 nm, respectively. Fig. 4 shows SEM micrographs of  $R_v$  composite samples. As can be seen from figure, two phases are well distributed, and the grain size is about 50 – 100 nm.

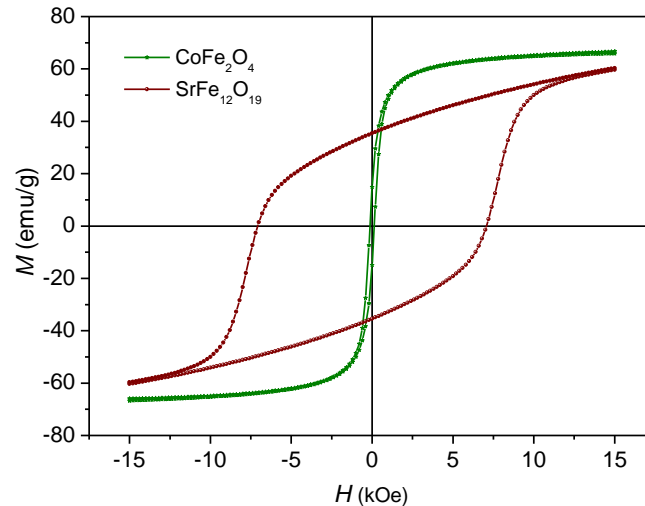


Figure 5. Hysteresis loops of the SrFe<sub>12</sub>O<sub>19</sub> and CoFe<sub>2</sub>O<sub>4</sub> samples annealed at 850 °C for 5 h.

Figure 5 depicts the hysteresis loops at room temperature of SrFe<sub>12</sub>O<sub>19</sub> and CoFe<sub>2</sub>O<sub>4</sub> nanoparticles. The SrFe<sub>12</sub>O<sub>19</sub> nanoparticles exhibit a magnetically hard behavior with the coercivity of 7 kOe and saturation magnetization of 60 emu/g. The hysteresis loop of CoFe<sub>2</sub>O<sub>4</sub> nanoparticles shows a magnetically soft behavior with the intrinsic coercivity of 0.314 kOe and saturation magnetization of 66 emu/g. It has been reported that the theoretical value of saturation magnetization for SrFe<sub>12</sub>O<sub>19</sub> and CoFe<sub>2</sub>O<sub>4</sub> is 74 emu/g and 91 emu/g, respectively. As seen in the Fig. 6a, the samples  $R_{m11}$  and  $R_{m17}$  exhibit a smooth hysteresis loop and show a single-phase magnetization behavior, although their crystallographically compose of two phases. While  $R_{m13}$  and  $R_{m15}$ , the hysteresis loop exhibits a typical “bee waist”. These results were in agreement with those reported by Moon K. W et. al [15]. In this study, the BaM+ x%NiZnFe<sub>2</sub>O<sub>4</sub> nanocomposite particles were fabricated by a self-propagating combustion method. As can be seen, the coercivity  $H_C$  decrease with decreasing concentration of SrFe<sub>12</sub>O<sub>19</sub>. It may be due to the fact the  $H_C$  of CoFe<sub>2</sub>O<sub>4</sub> is smaller than that of SrFe<sub>12</sub>O<sub>19</sub>. The magnetization  $M$  of  $R_{m11}$  and  $R_{m13}$  are comparatively larger as compared with that of SrFe<sub>12</sub>O<sub>19</sub> sample, owing to the present of CoFe<sub>2</sub>O<sub>4</sub> phase. However, for  $R_{m15}$  and  $R_{m17}$ , the value of magnetization  $M$  reduce tendency. The non-homogeneous distribution of phases can be a reason for the change of magnetization  $M$ . Thus, physical mixing method is an inadequate method for obtaining exchange-spring magnets because of non-homogenous distribution of magnetic phases (Fig. 3).

All the samples  $R_v$  show an excellent smooth hysteresis loop and a single – phase magnetization behavior. It indicates the hard and soft magnetic phases are switching individually due to the incomplete exchange-coupling [16-17]. The magnetization at 10 T ( $M$ ), remanence magnetization ( $M_r$ ) and coercivity ( $H_c$ ) obtained from hysteresis loops are showed in Table 2.

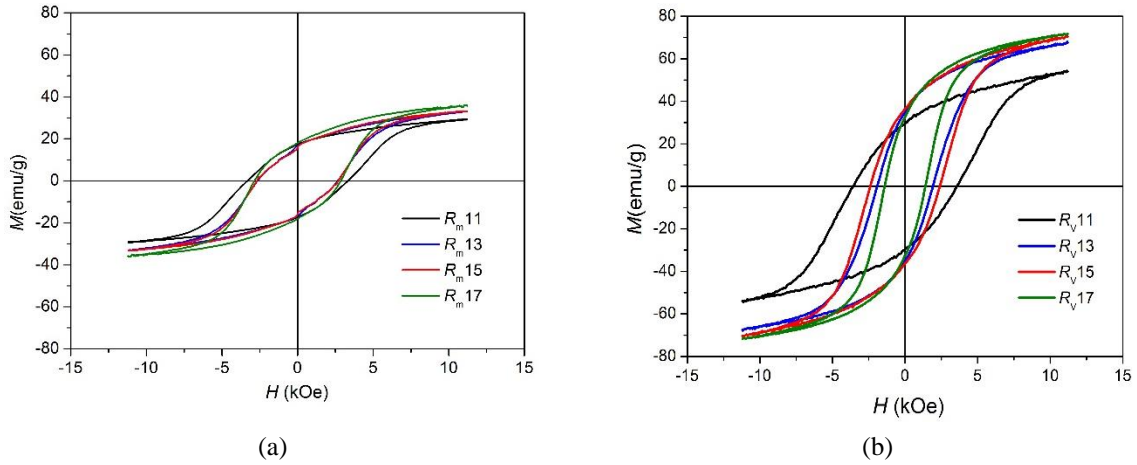


Figure 6. Hysteresis loops of the SrFe<sub>12</sub>O<sub>19</sub>/CoFe<sub>2</sub>O<sub>4</sub> nanocomposite samples (a)  $R_m$  and (b)  $R_v$  calcination at 850 °C for 5 hours.

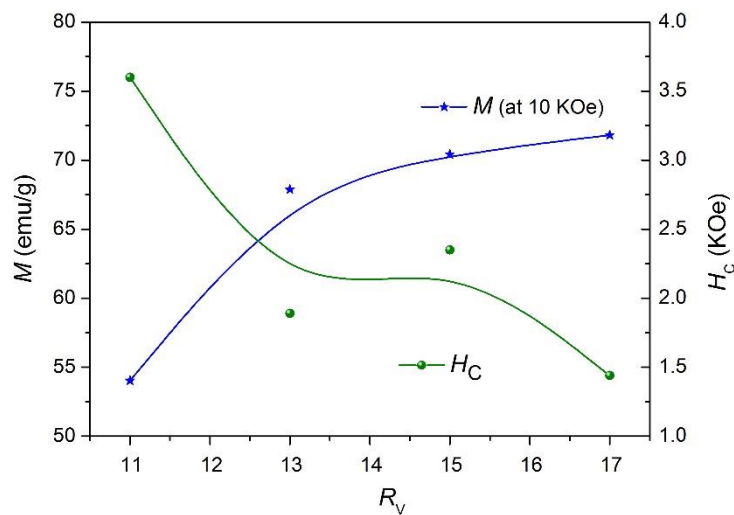


Figure 7. The variation in magnetization  $M$  (at 10 kOe) and coercive force ( $H_c$ ) with decreasing of the volume ratio  $R_v$ .

The dependence of magnetization  $M$  (at 10 kOe) and coercivity  $H_c$  on ratio  $R_v$  is shown in Fig. 7. As expected, the magnetic properties of nanocomposite particles can be enhanced with a strong exchange coupling. However, we can see that the coercive force decreases with increasing concentration of soft magnetically phase CoFe<sub>2</sub>O<sub>4</sub>. As concentration of the soft phase increases, the role of dipolar interactions among the soft grains becomes more important [18] and the reverse domains in soft phase with low nucleation field nucleate readily. Thus, the value of  $H_c$  decreases. In addition, the presence of  $\alpha$ -Fe<sub>2</sub>O<sub>3</sub> phase could be a reason for the decreasing of coercivity. This result has been found in the SrFe<sub>12</sub>O<sub>19</sub>/CoFe<sub>2</sub>O<sub>4</sub> [17], BaFe<sub>12</sub>O<sub>19</sub>/Fe<sub>3</sub>O<sub>4</sub> [19] and BaFe<sub>12</sub>O<sub>19</sub>/Ni<sub>0.5</sub>Zn<sub>0.5</sub>Fe<sub>2</sub>O<sub>4</sub> [20]. The value of coercivity  $H_c$  markedly decreases from 3.6 kOe to 1.44 kOe while the magnetization  $M$  increases from 54.02 emu/g to 71.81 emu/g when the ratio  $R_v$  decreases from 1:1 to 1:7 (table 2). The magnetization  $M$



of  $R_V17$  is larger about 8% and 19.6% than that of  $\text{CoFe}_2\text{O}_4$  and  $\text{SrFe}_{12}\text{O}_{19}$ , respectively. Compare with  $R_m$  samples, the magnetization  $M$  of  $R_V$  samples is higher than that of  $R_m$  samples. The enhancement of magnetization can be assigned to the homogeneously distributed phases and the improving of exchange interaction between the hard and soft grains.

Table 2. Magnetization at 10 kOe ( $M$ ), coercive force ( $H_C$ ) and remanence magnetization ( $M_r$ ) at room temperature of the  $\text{SrFe}_{12}\text{O}_{19}/\text{NiFe}_2\text{O}_4$  nanocomposite powders with different ratios  $R_m, R_V$ .

Sample	$H_C$ (kOe)	$M$ at 10 kOe (emu/g)	$M_r$ (emu/g)
$R_m11$	3.32	64	35.92
$R_m13$	2.69	62.89	32.28
$R_m15$	2.69	33.18	16.62
$R_m17$	2.92	36.05	18.19
$R_V11$	3.6	54.02	28.92
$R_V13$	1.89	67.87	34.21
$R_V15$	2.35	70.42	35.91
$R_V17$	1.44	71.81	33.17

#### 4. Conclusions

In summary, the  $\text{SrFe}_{12}\text{O}_{19}/\text{CoFe}_2\text{O}_4$  nanocomposites with exchange coupling behavior have been prepared successfully by sol gel method. XRD patterns confirmed the coexistence of two hard and soft phases together with a small amount of impurity phase of  $\alpha\text{-Fe}_2\text{O}_3$ . Nanocomposites prepared by physical mixing method, showed a typical “bee waist” type hysteresis loop and non-homogenous formation of two phases. The SEM micrographs of nanocomposites  $R_V$  showed homogenous formation of two phases and particle size distribution is about 50 – 100 nm. The hysteresis loop of the samples  $R_V$  behaves like a single magnetic phase, indicating a strong exchange coupling between two magnetically phases. The coercivity  $H_c$  decreases from 3.6 kOe to 1.44 kOe and the magnetization  $M$  increases from 54 to 71.81 emu/g with decreasing of ratio volume  $R_V$  from 1/1 to 1/7.

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